



## Performance & Design Analysis of forced Draft counter to cross flow Air cooled heat exchanger at extremely low ambient temperature i.e. at -28°C

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**ABSTRACT:** There are several sites, in the world as well as in India, where the ambient temperature reaches below 0°C to -28°C, at this temperature the fluid in heat exchanger freezes. If the fluid Freezes in Heat Exchanger, the heat exchanger ceases and it would damage the heat exchanger also. In extremely cold environments, overcooling of the process fluid may cause freezing. This may lead to tube burst, and hence protection from freezing is required to prevent plugging or damaging the tubes [2]. Heat Exchanger is designed on the basis of hot fluid temperature, cold fluid temperature & ambient temperature, but in practical sense, the ambient temperature changes throughout the year. Here we are analyzing the effect of extreme low ambient temperature on Forced Draft Counter to Cross flow Air Cooled Heat Exchanger. Here, we have taken the temperature of surrounding air, as -28°C. Here, we are studying the performance & design analysis of Air Cooled heat exchanger at extremely low ambient temperature. In this we are doing the thermal design of forced draft counters to cross flow Air Cooled heat exchanger at extremely low ambient temperature i.e. at -28°C. The most important parameter, while taking into consideration of designing Air Cooled Heat Exchanger is permissible /minimum tube skin temperature. There are various fluids such as Diethanolamine or Lean DEA which are used in various industries like oil Refinery, the temperature at which this fluid starts freezes is 9°C. So, as to protect the fluid from freezing, we need an equipment which maintains the temperature of ambient air & fluid according to their pour point & freezing temperature. For this, we can use the steam coil to raise the temperature of ambient air & fluid. If the fluid Freezes in Heat Exchanger, the heat exchanger ceases and it will damage the heat exchanger also. For this reason, we use the steam coil.

**Keywords:** Thermal Design, counter to cross flow heat exchanger, permissible/minimum tube skin temperature, lean dea, extremely low ambient temperature

### I. INTRODUCTION

Heat Exchanger is designed on the basis of hot fluid temperature, cold fluid temperature & ambient temperature, but in practical sense, the ambient temperature changes throughout the year. There are several sites, in India as well as in world, where the ambient temperature reaches below 0°C, that is freezing temperature. We know that in extreme low ambient temperature the fluid in the Air cooled heat exchanger freezes & this may lead to the tube burst & fluid freeze. At low ambient temperature the fluid in heat exchanger freezes. If the fluid Freezes in Heat Exchanger, the heat exchanger ceases and it would damage the heat

exchanger also. In extremely cold environments, overcooling of the process fluid may cause freezing. There are various fluids such as Diethanolamine or Lean DEA are used in Refinery, the temperature at which this fluid starts freezes is 9°C. So, as to protect the fluid from freezing

**The process parameters/boundary conditions for thermal design of Air Cooled heat Exchanger are-**

Flow rate of hot & cold fluid

Inlet & outlet temperature of hot & cold fluid

Inlet temperature of cold fluid

Allowable pressure drop [1]

## II. OBJECTIVES

1. The main objective of this master thesis is to give the idea for thermal design of Forced Draft Counter to Cross Flow Air Cooled Heat Exchanger at extremely low ambient temperature, as there are lots of problems associated, while designing an Air Cooled Heat Exchanger.
2. In this research paper we will analyze the effect of ambient temperature on Forced Draft Counter to Cross flow Air Cooled Heat Exchanger. Here, we have taken the temperature of surrounding air, as  $-28^{\circ}\text{C}$ . Here, we are studying the performance & design analysis of Air Cooled heat exchanger at extremely low ambient temperature.
3. To give the thermal design & procedure of Air cooled heat exchanger counter to cross flow at extremely low ambient temperature.
4. To discuss the various challenges while designing the Counter to Cross Flow Heat Exchanger.

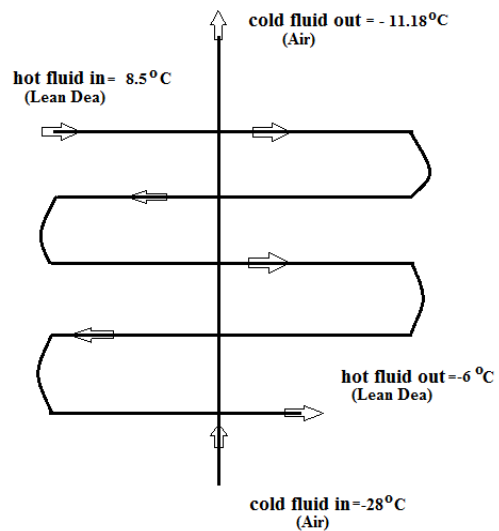
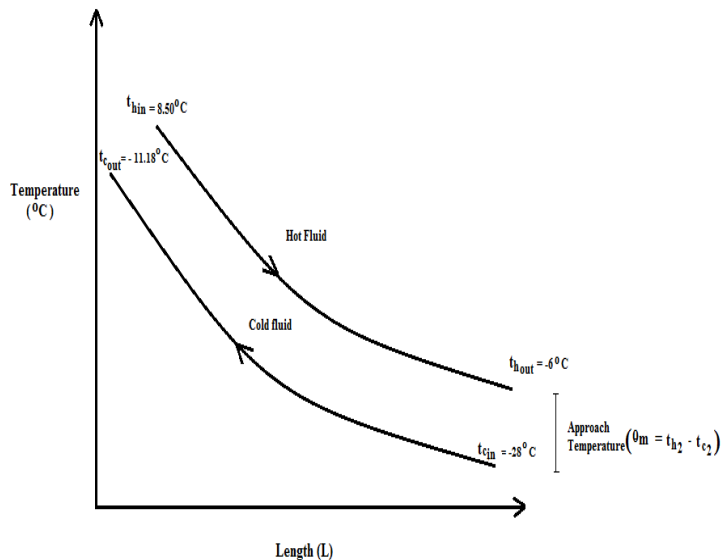
### Thermal Design of forced draft counter to cross flow heat exchanger for extremely low ambient condition, i.e. $-28^{\circ}\text{C}$

In this we are doing & analyzing the thermal design of forced draft counters to cross flow Air Cooled heat exchanger at extremely low ambient temperature i.e. at  $-28^{\circ}\text{C}$ . The most important parameter, while taking into consideration of designing Air Cooled Heat Exchanger is permissible /minimum tube skin temperature At this, the temperature of surrounding air, i.e. temperature of cold fluid (air) is  $-28^{\circ}\text{C}$ . Here we have gone to

extremely low ambient temperature i.e.  $-28^{\circ}\text{C}$ , By previous records of temperature on some particular locations, we have come to the conclusion that in extreme cases, the temperature of these locations falls to  $-28^{\circ}\text{C}$ . In this we have done the thermal design & performance analysis of forced draft counter to cross flow air heat exchanger at extremely low ambient conditions, so we have taken  $-28^{\circ}\text{C}$  temperature for designing & performance analysis of Air Cooled Heat Exchanger. The most important parameter, while taking into consideration of designing Air Cooled Heat Exchanger is permissible /minimum tube skin temperature. In this forced draft counter to cross flow air cooled heat exchanger, the process fluid is lean dea. The pour point of any fluid can be defined as that point, when fluid ceases to flow i.e. fluid start freezing at this temperature

**For extremely low atmospheric conditions, i.e. extremely low ambient temperature is-  $-28^{\circ}\text{C}$ , the process parameters are-**

- a). Flow rate of hot fluid (lean dea) = 94.526 (1000-kg/h)
- b). Flow rate of cold fluid (air) = 300.262 (1000-kg/h)
- c). Inlet temperature of hot fluid =  $8.5^{\circ}\text{C}$
- d). Outlet temperature of hot fluid =  $-6^{\circ}\text{C}$
- e). Inlet temperature of cold fluid (air) =  $-28^{\circ}\text{C}$
- f). Allowable pressure drop of hot fluid =  $0.710\text{kgf/cm}^2$
- g). Inlet pressure of hot fluid =  $2.133\text{kgf/cm}^2$
- h). Altitude



### Nomenclature:

- Hot fluid (lean dea) enters in Air Cooled Heat Exchanger =  $t_{hin} = 8.5^{\circ}\text{C}$   
 Hot fluid (lean dea) leaves the Air Cooled Heat Exchanger =  $t_{hout} = -6^{\circ}\text{C}$   
 Cold fluid (air) enters in Air Cooled Heat Exchanger =  $t_{cin} = -28^{\circ}\text{C}$   
 Cold fluid (air) leaves the Air Cooled Heat Exchanger =  $t_{cout} = -11.18^{\circ}\text{C}$

Change in hot fluid(lean dea) temperature  $\Delta t_h = t_{hin} - t_{hout} = 8.5^\circ\text{C} - (-6^\circ\text{C}) = 14.5^\circ\text{C}$

Change in cold fluid (air) temperature  $\Delta t_c = t_{cout} - t_{cin} = -11.18 - (-28) = 16.82^\circ\text{C}$

Approach Temperature =  $\theta_{m1} = t_{hout} - t_{cin} = -6^\circ\text{C} - (-28^\circ\text{C}) = 22^\circ\text{C}$

Approach Temperature =  $\theta_{m2} = t_{hin} - t_{cout} = 8.5^\circ\text{C} - (-11.18^\circ\text{C}) = 19.68^\circ\text{C}$

There are two different approach temperatures, but in counter to cross flow heat exchanger, we consider the

Approach Temperature =  $\theta_{m1} = t_{hout} - t_{cin} = -6^\circ\text{C} - (-28^\circ\text{C}) = 22^\circ\text{C}$

Only this approach temperature is important, while designing the forced draft counter to cross flow heat exchanger.

The most important parameter, while taking into consideration of designing of Air Cooled Heat Exchanger is Tube skin temperature. In this Forced draft counter to cross flow Air Cooled heat exchanger the process fluid is lean dea. We know that, the pour point of lean dea is  $8^\circ\text{C}$  and as per API 661 guidelines of heat exchanger design,

The permissible tube skin temperature = pour point of fluid +  $9^\circ\text{C}$

$= 8^\circ\text{C} + 9^\circ\text{C}$

$= 17^\circ\text{C}$

So, permissible tube skin temperature of Air Cooled Heat Exchanger is  $17^\circ\text{C}$ , but in this case it goes to  $-12.73^\circ\text{C}$ , in such condition fluid in the heat exchanger ceases resulting in exchanger failure & tube bursts .So, this design of Air Cooled Heat Exchanger is Unsafe & Fail.

By using thermal design software we found the following properties of hot fluid (lean dea) & cold fluid (Air)-  
Stream properties of hot fluid side fluid (lean dea) –

Stream Properties						
Rating-Horizontal air-cooled heat exchanger forced draft countercurrent to crossflow						MKH Units
Hot Tubeside Fluid	Inlet			Outlet		
Fluid name	Lean DEA					
Temperature (C)	8.50			-6.00		
Pressure (kgf/cm2A)	2.133			1.318		
Weight fraction vapor (--)	0.0000			0.0000		
Vapor Properties						
Density (kg/m3)	--			--		
Viscosity (cP)	--			--		
Conductivity (kcal/hr-m-C)	--			--		
Heat capacity (kcal/kg-C)	--			--		
Molecular weight (--)	--			--		
Liquid Properties						
Density (kg/m3)	1044.53			1053.83		
Viscosity (cP)	4.1136			6.6665		
Conductivity (kcal/hr-m-C)	0.4019			0.3929		
Heat capacity (kcal/kg-C)	0.8877			0.8817		
Molecular weight (--)	0			0		
Latent heat (kcal/kg)	--			--		
Surface tension (dyne/cm)	0.0000			0.0000		
Molar Composition				Vapor	Liquid	K-Value
1 [New User-Defined]	--	--	--	--	--	--

Stream properties of cold outside fluid (Air)

Stream Properties						
Rating-Horizontal air-cooled heat exchanger forced draft countercurrent to crossflow						MKH Units
Cold Outside Fluid	Inlet			Outlet		
Fluid name						
Temperature (C)	-28.00			-11.18		
Pressure (kgf/cm2A)	1.031			1.030		
Weight fraction vapor (--)	1.0000			1.0000		
Vapor Properties						
Density (kg/m3)	1.4373			1.3450		
Viscosity (cP)	0.0158			0.0166		
Conductivity (kcal/hr-m-C)	0.0189			0.0200		
Heat capacity (kcal/kg-C)	0.2401			0.2401		
Molecular weight (--)	28.96			28.96		
Liquid Properties						
Density (kg/m3)	--			--		
Viscosity (cP)	--			--		
Conductivity (kcal/hr-m-C)	--			--		
Heat capacity (kcal/kg-C)	--			--		
Molecular weight (--)	--			--		
Latent heat (kcal/kg)	--			--		
Surface tension (dyne/cm)	--			--		
Molar Composition	Vapor	Liquid	K-Value	Vapor	Liquid	K-Value





## III. RESULTS

Output Summary							
						MKH Units	
Rating-Horizontal air-cooled heat exchanger forced draft countercurrent to crossflow							
Process Conditions			Outside		Tubeside		
Fluid name					Lean DEA		
Fluid condition			Sens. Gas		Sens. Liquid		
Total flow rate (1000-kg/hr)			300.262		94.526		
Weight fraction vapor, In/Out			1.000	1.000	0.000	0.000	
Temperature, In/Out (Deg C)			-28.00	-11.18	8.50	-6.00	
Skin temperature, Min/Max (Deg C)			-17.74	-1.89	-12.73	3.55	
Pressure, Inlet/Outlet (kgf/cm2A)			1.031	1.030	2.133	1.318	
Pressure drop, Total/Allow (mmH2O) (kgf/cm2)			10.840	0.000	0.815	0.710	
Midpoint velocity (m/s)			5.42		1.42		
- In/Out (m/s)					1.43	1.47	
Heat transfer safety factor (--)			1		1		
Fouling (m2-hr-C/kcal)			0.000000		0.000500		
Exchanger Performance							
Outside film coef (kcal/m2-hr-C)			37.33		Actual U (kcal/m2-hr-C)	17.339	
Tubeside film coef (kcal/m2-hr-C)			1702.55		Required U (kcal/m2-hr-C)	20.850	
Clean coef (kcal/m2-hr-C)			22.743		Area (m2)	2811.99	
Hot regime			Sens. Liquid		Overdesign (%)	-16.84	
Cold regime			Sens. Gas				
EMTD (Deg C)			20.7				
Duty (MM kcal/hr)			1.212				
Unit Geometry				Tube Geometry			
Bays in parallel per unit			1		Tube type	High-finned	
Bundles parallel per bay			2		Tube OD (mm)	25.400	
Extended area (m2)			2811.99		Tube ID (mm)	21.184	
Bare area (m2)			123.118		Length (mm)	7999.903	
Bundle width (mm)			1276.		Area ratio(out/in) (--)	27.3853	
Nozzle			Inlet	Outlet	Layout	Staggered	
Number (--)			1	1	Trans pitch (mm)	75.000	
Diameter (mm)			131.750	131.750	Long pitch (mm)	64.950	
Velocity (m/s)			0.92	0.91	Number of passes (--)	4	
R-V-SQ (kg/m-s2)			887.83	879.99	Number of rows (--)	6	
Pressure drop (kgf/cm2)			4.980e-3	3.141e-3	Tubecount (--)	99	
					Tubecount Odd/Even (--)	17 / 16	
					Tube material	Carbon steel	
Fan Geometry				Fin Geometry			
No/bay (--)			2		Type	Plain round	
Fan ring type			30 deg		Fins/length fin/meter	433.0	
Diameter (mm)			2286.		Fin root mm	27.000	
Ratio, Fan/bundle face area (--)			0.40		Height mm	15.075	
Driver power (kW)			6.34		Base thickness mm	0.400	
Tip clearance (mm)			11.430		Over fin mm	57.150	
Efficiency (%)			65		Efficiency (%)	81.5	
Airside Velocities			Actual	Standard	Area ratio (fin/bare) (--)	22.8398	
Face (m/s)			2.84	3.40	Material	Aluminum 1060 - H14	
Maximum (m/s)			5.27	6.31	Thermal Resistance, %		
Flow (100 m3/min)			34.818	41.654	Air	46.45	
Velocity pressure (mmH2O)			3.670		Tube	27.89	
Bundle pressure drop (mmH2O)			9.263		Fouling	23.76	
Bundle flow fraction (--)			1.000		Metal	1.90	
					Bond	0.00	
Bundle 85.45			Airside Pressure Drop, %			Louvers	6.03
Ground clearance 0.00			Fan guard	0.55	Hail screen	0.00	
Fan ring 2.03			Fan area blockage	5.94	Steam coil	0.00	

Final Results									
Rating-Horizontal air-cooled heat exchanger forced draft countercurrent to crossflow									
MKH Units									
Process Data			Airside		Tubeside				
Fluid name					Lean DEA				
Fluid condition			Sens. Gas		Sens. Liquid				
Total flow rate (1000-kg/hr)			300.262		94.526				
Weight fraction vapor, In/Out (--)			1.000	1.000	0.000	0.000			
Temperature, In/Out (Deg C)			-28.00	-11.18	8.50	-6.00			
Skin temperature, Min/Max (Deg C)			-17.74	-1.89	-12.73	3.55			
Wall temperature, Min/Max (Deg C)			-17.74	-1.89	-12.89	3.36			
Pressure, In/Out (kgf/cm2A)			1.031	1.030	2.133	1.318			
Pressure drop, Total/Allowed (mmH2O) (kgf/cm2)			10.840	0.000	0.815	0.710			
Pressure Drop, A-frame reflux section (kgf/cm2)									
Velocity - Midpoint (m/s)			5.42		1.42				
- In/Out (m/s)					1.43	1.47			
Film coefficient, Bare/Extended (kcal/m2-hr-C)			852.58	37.33	1702.55				
Mole fraction inert (--)									
Heat transfer safety factor (--)			1		1				
Fouling resistance (m2-hr-C/kcal)			0.000000		0.000500				
Overall Performance Data									
Overall coef, Design/Clean/Actual (kcal/m2-hr-C)			20.850	/	22.743	/	17.339		
Heat duty, Calculated/Specified (MM kcal/hr)			1.2118	/	0.0000				
Effective mean temperature difference (Deg C)			20.67						
Unit and Bundle Construction Information									
Bays in parallel/unit (--)			1	Bundles in parallel/bay			2		
Extended area/unit (m2)			2811.99	Bare area/unit (m2)			123.118		
Extended area/bundle (m2)			1405.99	Bare area/bundle (m2)			61.559		
Tubepasses/Tuberows (--)			4 /	6	Number of tubes/bundle (--)			99	
Tube count, Odd rows/Even rows (--)			17 /	16	Edge seals (--)			Yes	
Bundle width (mm)			1276.		Fan guard (--)			Yes	
Clearance (mm)			9.525		Louvers (--)			Yes	
Header depth (mm)			101.600		Steam coil (--)			No	
Header Box						Hail screen (--)			No
- Plate thickness (mm)			25.400		Tube support information				
- Tubesheet thickness (mm)			34.925		- Number (--)			4	
Plenum type			Tapered		- Width (mm)			25.400	
Weight/Bundle (kg)			3649		Orientation (from horiz.) (deg)			0.00	
Structure weight (kg)			3347		Tubeside volume (L)			386.5	
Total weight, Dry / Wet (kg)			13165 /		13937				
Ladder/walkway weight (kg)			2520		Cost Factor (--)			47.3566	
Tube Information									
Straight length (mm)			8000.		Tube type			High-finned	
Unfinned length (mm)			36.000		Unheated length (mm)			171.450	
Layout (--)			Staggered		Area ratio (fin/bare) (--)			22.8398	
Transverse pitch (mm)			75.000		Fins per unit length (fin/meter)			433.0	
Longitudinal pitch (mm)			64.950		Fin root diameter (mm)			27.000	
Tube form (--)			Straight		Fin height (mm)			15.075	
Outside diameter (mm)			25.400		Fin thickness at base (mm)			0.400	
Inside diameter (mm)			21.184		Fin thickness at tip (mm)			0.189	
Area ratio (out/in) (--)			27.3853		Fin type (--)			Plain round	
Over fin diameter (mm)			57.150		Fin efficiency (%)			81.5	
Tube material			Carbon steel		Internal tube type			None	
Fin material			Aluminum 1060 - H14						

Final Results				
MKH Units				
Rating-Horizontal air-cooled heat exchanger forced draft countercurrent to crossflow				
Inlet Airside Velocities			Actual	Standard
Face velocity	(m/s)		2.84	3.40
Maximum velocity	(m/s)		5.27	6.31
Volumetric flow	(100 m3/min)		34.818	41.654
Maximum mass velocity	(kg/s-m2)		7.575	
Air humidity	(%)			
Volumetric flow per fan at fan inlet	(100 m3/min)		17.409	
Velocity at fan inlet	(m/s)		7.07	
Fan Description and Fan Power				
Number of fans per bay	(--)			2
Diameter	(mm)			2286.
Tip clearance	(mm)			11.430
Ratio, fan area to bay face area	(--)			0.40
Fan ring type	(--)			30 deg
Percent open area	- in fan guard	(%)		95
	- in hail screen	(%)		0
Ratio, ground clearance to fan diameter	(--)			
Percent blockage, other obstruction	(%)			5
Bundle pressure drop/ Velocity pressure	(mmH2O)		9.263 /	3.670
Fan and drive efficiency	(%)			65
Motor power per fan-design air temperature	(kW)			6.34
Motor power per fan-minimum air temperature	(kW)			0.00
Ambient temperature, maximum / minimum	(Deg C)		-17.78 /	-17.78
Two-Phase Parameters				
Method	Inlet	Center	Outlet	Mix F
Bundle flow fraction	(--)	1.000		
Heat Transfer and Pressure Drop Parameters			Tubeside	Outside
Midpoint j-factor			(--)	0.0058
Heat transfer		Wall Correction	(--)	0.9680
		Row Correction	(--)	1.0000
Midpoint f-factor			(--)	0.0105
Pressure drop		Wall Correction	(--)	1.0488
		Row Correction	(--)	1.0008
Reynolds number		Inlet	(--)	7670
		Midpoint	(--)	5686
		Outlet	(--)	4930
Fouling layer thickness			(mm)	0.000
Input minimum velocity			(m/s)	
Input maximum velocity			(m/s)	
Input minimum wall temperature			(Deg C)	
Input maximum wall temperature			(Deg C)	
Thermal Resistance (Percent)				Over Design
Air	Tube	Fouling	Metal	Bond
46.45	27.89	23.76	1.90	0.00
				-16.84
Airside Pressure Drop (Percent)				
Across bundle		85.45	Other obstruction	5.94
Fan ring		2.03	Steam coil	0.00
Fan guard		0.55	Louvers	6.03
Ground clearance		0.00		
Tube Nozzle (Perpendicular)		Inlet	Outlet	
Number of nozzles	(--)	1	1	
Diameter	(mm)	131.750	131.750	
Velocity	(m/s)	0.92	0.91	
Nozzle R-V-SQ	(kg/m-s2)	887.83	879.99	
Pressure drop	(kgf/cm2)	4.980e-3	3.141e-3	



#### IV. CONCLUSION AND OUTCOME

The most important parameter, while taking into consideration for designing the Forced Draft Counter to cross flow Air Cooled Heat Exchanger is tube skin temperature. In this Forced Draft Counter to cross flow Air Cooled Heat Exchanger, the process fluid is lean dea. Here, the air acts as a cold fluid & lean dea acts as a hot fluid. The hot fluid lean dea loses its heat from 8.5°C to -6°C & cold fluid air gains the heat from -28°C to -11.18°C, during heat exchanging process. By studying the various properties of lean dea, we come to know that the pour point of lean dea is 8°C & by studying API 661 guidelines for designing of Air Cooled Heat Exchanger, the minimum tube skin temperature is equal to the pour point of fluid +9°C API Margin.

i.e. Permissible/minimum tube skin temperature =  
pour point of fluid (lean dea) +9°C (API Margin)  
= 8°C +9°C = 17°C

By studying the properties of lean dea we come to know that the tube skin temperature at -28°C is -12.73°C. At -28°C the permissible tube skin temperature is -12.73°C, which is far below than the permissible tube skin temperature (17°C). So, the design & performance of Forced Draft Counter to Cross Flow Air Cooled Heat Exchanger is unsafe & fail & this will lead to freezing of fluid & tube burst in the Air Cooled Heat Exchanger. So, for this reason a equipment or a method is needed for heating the process fluid and to maintain the temperature of tube skin as per API guidelines. In these ambient conditions, there is a need of steam coil because at this temperature, the fluid in the heat exchanger freezes, hence there is a problem in this design. So, we require a steam coil for heating the fluid, so that tube skin temperature is maintained at 17°C.

#### V. FUTURE SCOPE

For extremely low ambient temperature the fluid in the heat exchanger freezes for this A steam coil is required for heating the fluid, so that the tube skin temperature is maintained at 17°C. So we have to design a steam coil to prevent the fluid from freezing without affecting the performance of Air Cooled Counter to cross flow heat exchanger. And there arises a question that at what temperature we start the steam coil for heating the fluid to achieve maximum auxiliary power saving, energy saving & lower use of steam? In case if the fluid is

already freeze, than the fan, motor, pumps do the extra work for heating the fluid. This will lead to more power, more energy & more steam consumption.

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